

# Adaptive Force Control Solutions

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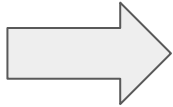
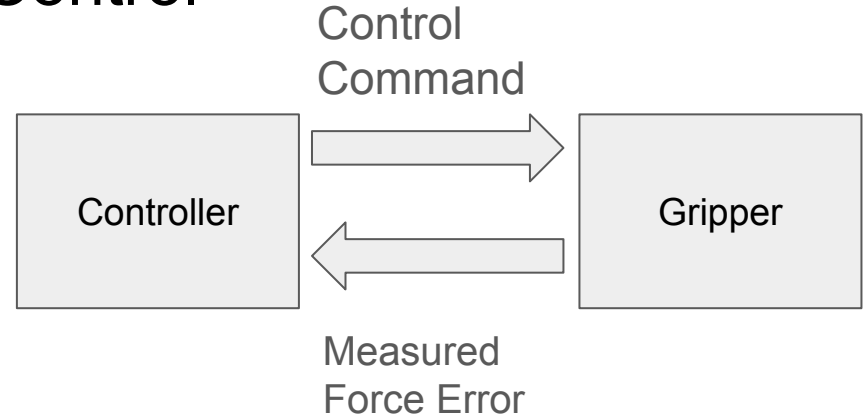


Universität Hamburg

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# Motivation - Adaptive Force Control

- Impedance Controller as classical real time Force controller
- Reacts only to measured Values



Idea : Predict parameters parameters

# Motivation - Problem Overshoot

- All Controllers that are based on measured values can produce overshoot
- Risk of destruction or slippage



Idea : Adaptive Force Control to predict future force

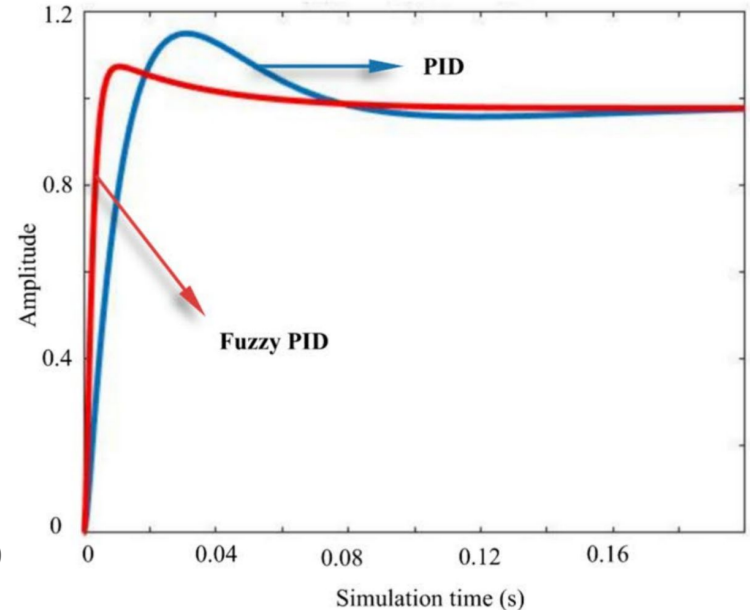


Figure in [2]

# Motivation - Force Oscillation

- Grippers Control Discretized
- Discrete Gripper Configuration Space

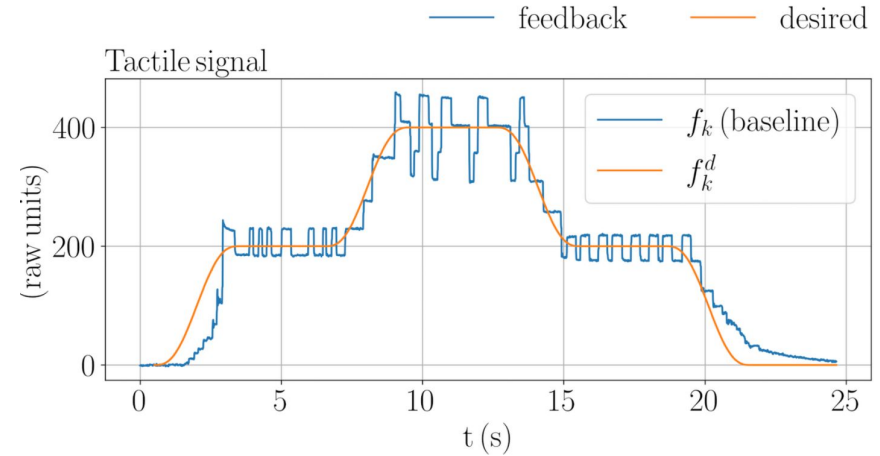


Figure [3]



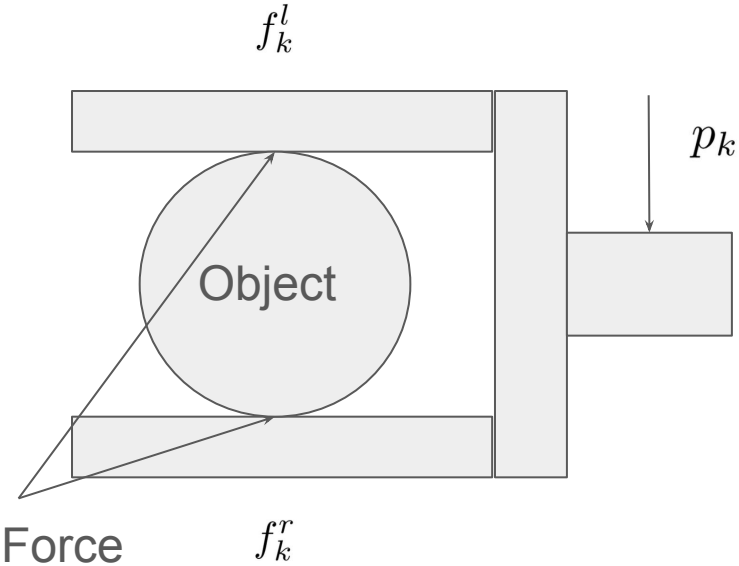
Target Forces of Controller may never be reached

# Modeling The Gripper

- 1 Degree of Freedom gripper at time  $k \in \mathbb{N}$
- Mean Tactile Force  $f_k = \frac{f_k^l + f_k^r}{2}$

- Discretized Gripper Aperture  $p_k = \left\lfloor \frac{u_k}{\delta_p} \right\rfloor \delta_p = N_k \delta_p$  Tactile Force Sensors

- Desired Continuous Aperture by Controller  $u_k \in \mathbb{R}$



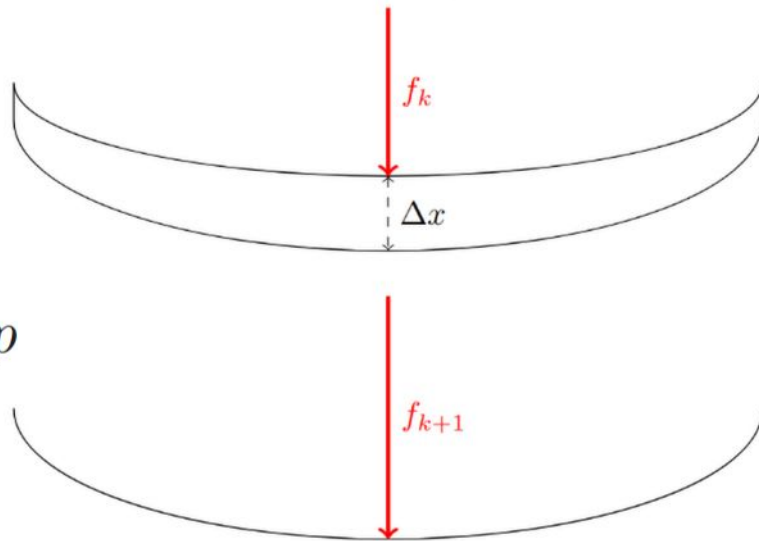
# Stiffness

- How an Object deforms under Force

$$s = \frac{f_{k+1} - f_k}{\Delta x}$$

- Linear Relation: Gripper Position  $\sim$  Output Force

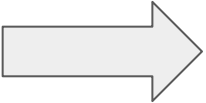
$$f(p) = c_0 + c_1 p$$



Relation is Material Dependent!

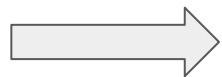
# Modeling the Controller

- Linear Relation  $f(p) = c_0 + c_1 p$
- Measured Error  $e_k = f_k^d - f_k$
- Next Controller aperture value  $u_{k+1} = u_k + k_i e_k \Delta_t$

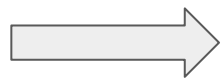
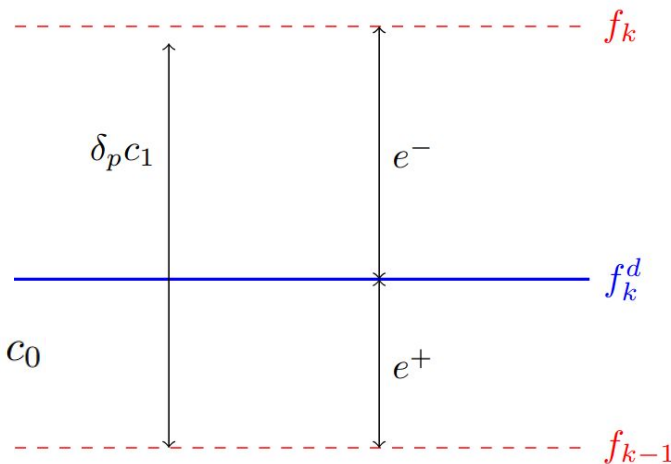

$$e_{k+1} = -c_1 \left[ \frac{u_k + k_i e_k \Delta_t}{\delta_p} \right] \delta_p + f_{k+1}^d - c_0$$

# Proof of Oscillation

System at Equilibrium  $e_{k+1} = e_k = e_{eq}$



From Controller Model  $e_{eq} = -c_1 \left[ \frac{u_{eq} + k_i e_{eq} \Delta_t}{\delta_p} \right] \delta_p + f_{eq}^d - c_0$



$e_{eq} = 0$  only if  $\left| \frac{f_{eq}^d - c_0}{c_1 \delta_p} \right| \in \mathbb{N}.$

# Solution: Adaptive Force Control

Adaptive Controller on  
Future Error

$$u_{k+1} = u_k + \Delta_u,$$

$$\Delta_u = \begin{cases} k_i e_k \Delta_t & |e_{k+1}^m| < |e_k| \\ 0 & \text{otherwise.} \end{cases}$$

Predict Future Error

$$e_{k+1}^m = f_{k+1}^d - f_{k+1}^m$$

$$\delta(e_k) = \text{sgn}(e_k) \left[ \frac{|e_k|}{c_1 \delta_p} \right] \delta_p$$

$$f_{k+1}^m = f(p_k + \delta(e_k))$$

# Measurement Prediction

$$f_{k+1}^m = f(p_k + \delta(e_k))$$

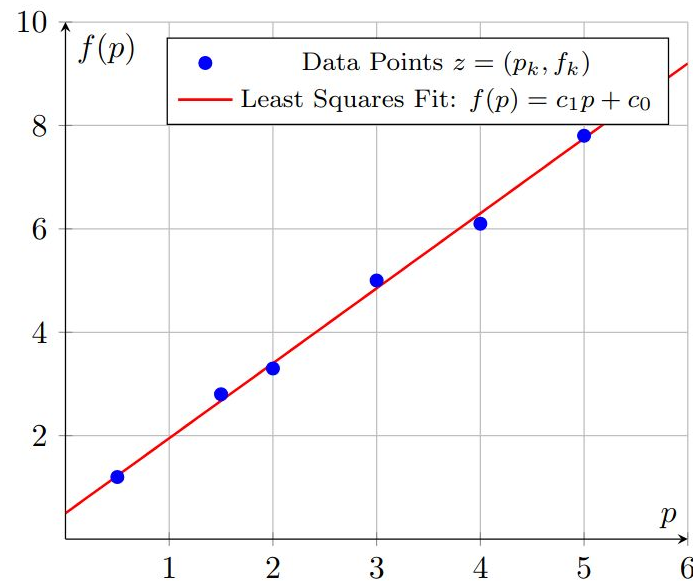


Requires Knowledge  
of Function  $f$



Linear Regression with  
Least Squares Error

$$z = (p_k, f_k)$$



$$f(p) = \sum_{i=0}^N c_i p^i$$

# Material Experiments

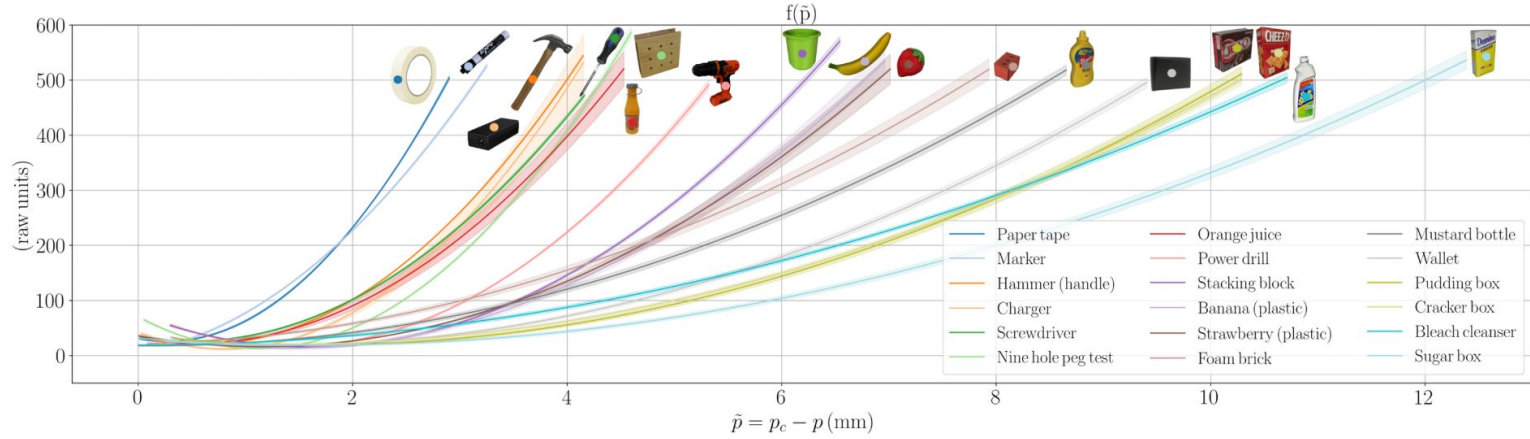


Figure [3]

[3] Nicola A Piga and Lorenzo Natale. "Adaptive tactile force control in a parallel gripper with low positioning resolution". In: IEEE Robotics and Automation Letters 8.9 (2023), pp. 5544–5551.

# Results

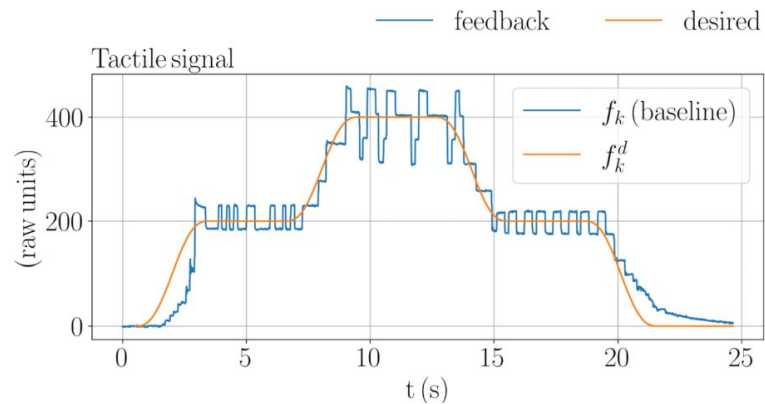


Figure [3]

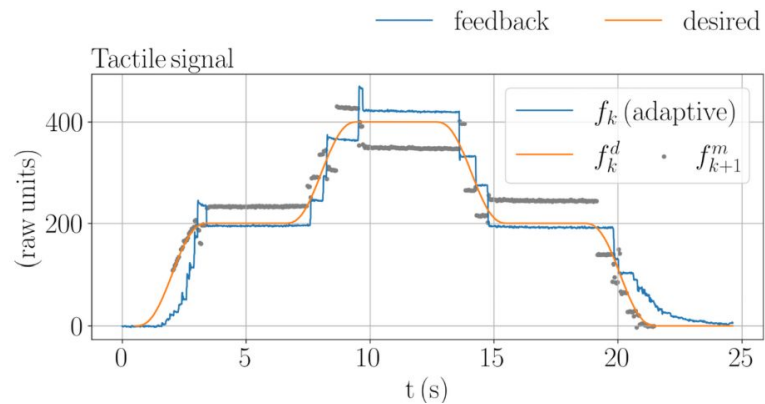
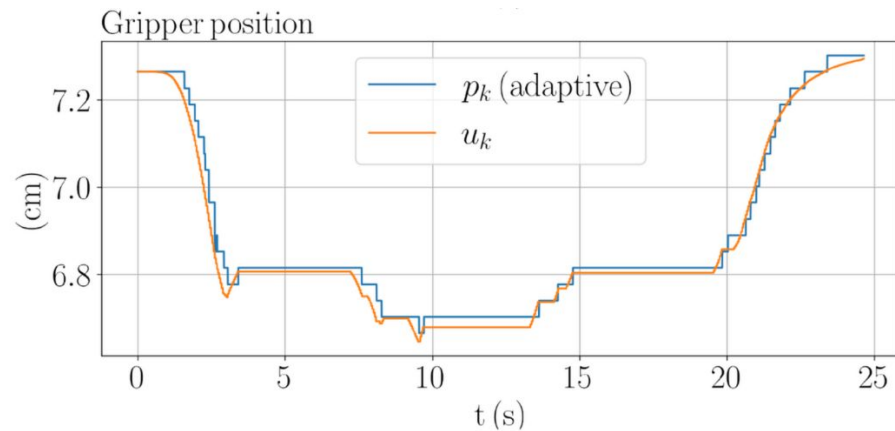
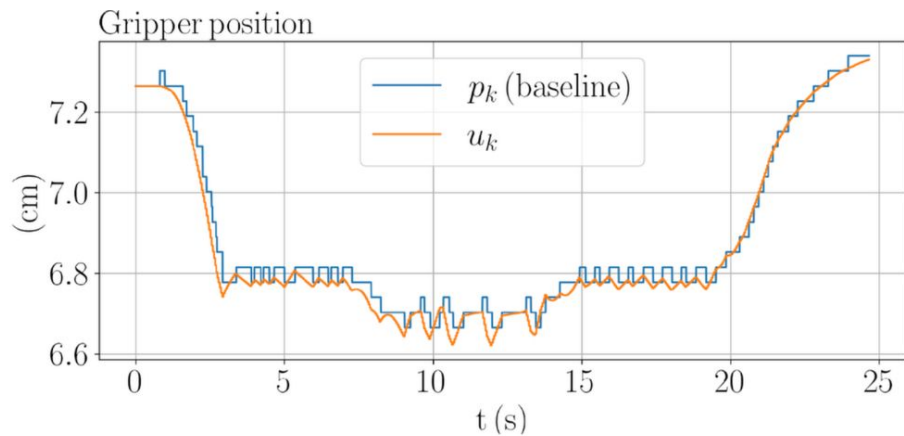


Figure [3]

# Results



# Conclusion

- Output Force Oscillation can be prevented
- Prediction of Future Error can prevent Overshoot

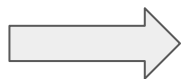
## Problems:

- Wrong Predictions can result in wrong Force Control
- The Selection of the Gain is Material Dependent

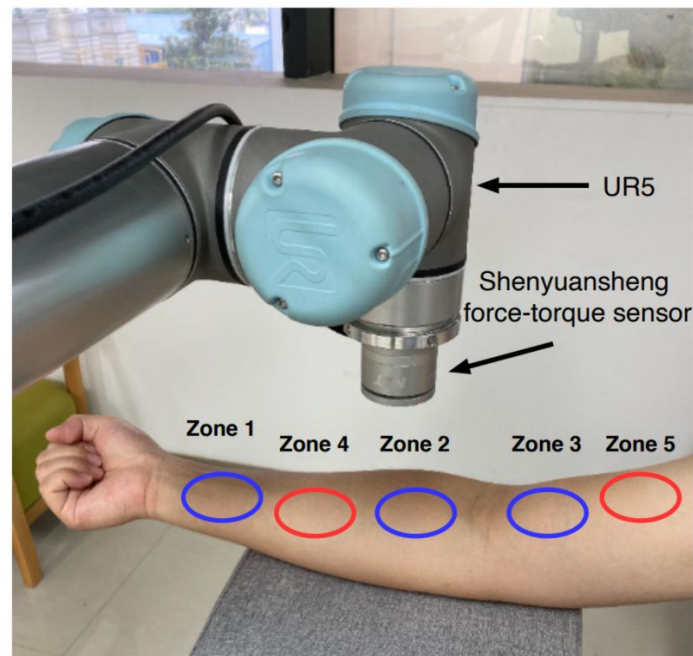
Questions?

# Changing Environments

- Force Control on Medical Robot critical
- No simple model for all regions of the human body



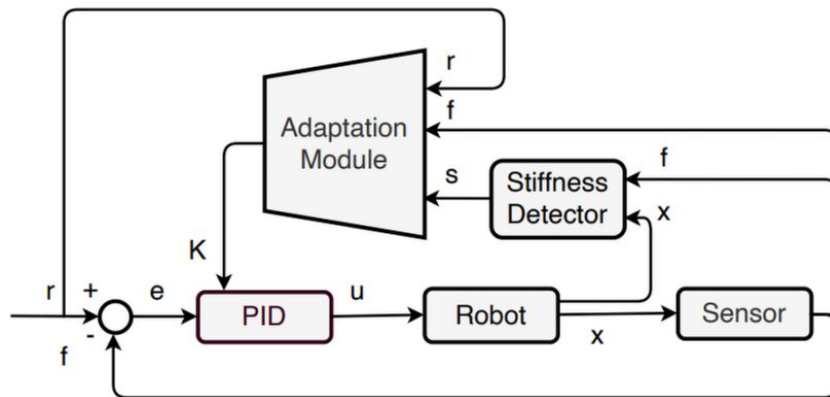
Adaptive Force Control



Zhaoxing Deng, Xutian Deng, and Miao Li. "Learning Based Adaptive Force Control of Robotic Manipulation Based on Real-Time Object Stiffness Detection". In: arXiv preprint arXiv:2109.06702 (2021) [4]

# Proposed Controller

- Basis is a PID controller
- PID controller parameters are set by Adaptation Modul
- Modul is a NN



## PID Force Controller:

Zhaoxing Deng, Xutian Deng, and Miao Li. "Learning Based Adaptive Force Control of Robotic Manipulation Based on Real-Time Object Stiffness Detection". In: arXiv preprint arXiv:2109.06702 (2021) [4]