# Introduction to Robotics 

## Lecture 5

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## Joint velocities $\Leftrightarrow$ End-effector velocities

## Jacobian

- Jacobian

$$
\delta x_{(m \times 1)}=J_{(m \times n)} \delta q_{(n \times 1)} \quad \text { where } \quad J_{i j}(q)=\frac{\partial}{\partial q_{j}} f_{i}(q)
$$

- Angular/Linear velocity Jacobian

$$
J=\left[\begin{array}{l}
J_{v} \\
J_{w}
\end{array}\right], \quad\left[\begin{array}{l}
{ }^{0} v_{n} \\
0 \\
\omega_{n}
\end{array}\right]=\left[\begin{array}{l}
J_{v} \\
J_{w}
\end{array}\right] \dot{q}
$$

- Computation of the final Jacobian
- Geometric singularities:
- for any two revolute joints, the joint axes are collinear
- any three parallel rotation axes lie in a plane
- any four rotational axes intersect at a point
- any three coplanar revolute axes intersect at a point
- Mathematical singularities:

$$
\operatorname{det} J=0 \Longrightarrow J \text { is not invertible }
$$

Where the determinant is equal to zero, the Jacobian has lost full rank and is singular.

## Outline

## Introduction

Spatial Description and Transformations
Forward Kinematics
Robot Description
Inverse Kinematics for Manipulators
Instantaneous Kinematics
Trajectory Generation 1
Trajectory and related concepts
Trajectory generation
Solutions of trajectory generation
Optimizing motion
Application
Trajectory Generation 2
Dynamics
Robot Control

## Outline (cont.)

Path Planning
Task/Manipulation Planning
Telerobotics
Architectures of Sensor-based Intelligent Systems
Summary
Conclusion and Outlook

## Definition

A trajectory is a time history of position, velocity and acceleration
for each DOF
Describes motion of TCP frame relative to base frame

- abstract from joint configuration
- Changes in position, velocity and acceleration of all joints are analyzed over a period of time
- Trajectory with $n$ DOF is a parameterized function $q(t)$ with values in its motion region.
- Trajectory $q(t)$ of a robot with $n$ DOF is then a vector of $n$ parameterized functions $q_{i}(t), i \in\{1 \ldots n\}$ with one common parameter $t$ :

$$
q(t)=\left[q_{1}(t), q_{2}(t), \ldots, q_{n}(t)\right]^{T}
$$

## Problem

The robot is at point $A$ and wants move to point $B$.

- How does the robot get to point B?
- How long does it take the left arm to get to point $B$ ?
- Which possible constraints exist for moving from $A$ to $B$ ?



## Problem

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- Which possible constraints exist for moving from $A$ to $B$ ?


## Solution

- generate a possible and smooth trajectory
- describe intermediate poses (waypoints)
- usually fixed temporal intervals
- obey the physical boundaries of the mechanics of the robot


Pick pos $_{\text {Start }}=$ object, vel $S_{\text {Start }}=0, a c c_{S t a r t}=0$
Lift-off limited velocity and acceleration
Motion continuous via waypoints, full velocity and acceleration Set-down similar to Lift-off

Place similar to Pick

Trajectory planning (cont.)
Trajectory Generation 1 - Trajectory and related concepts


UR10e arm, Shadow C5 hand, feed-forward policy, 10 demonstrations, video speed: 2.4


## Generation of trajectories

## Task

- find a smooth trajectory for moving the robot from start to goal pose
- use continuous functions of time
- A trajectory is $C^{k}$-continuous, if all derivatives up to the $k$-th (including) exist and are continuous.
- A trajectory is called smooth, if it is at least $C^{2}$-continuous
- $q(t)$ is the trajectory,
- $\dot{q}(t)$ is the velocity,
- $\ddot{q}(t)$ is the acceleration,
- $\dddot{q}(t)$ is the jerk



## Task

- find trajectory for moving the robot from start to goal pose
- use continuous functions of time

Representation solution:

- calculation of Cartesian trajectories for the TCP
- calculation for trajectories in joint space


## Generation of trajectories (cont.)



Pouring setup


Pushing setup


Disadvantages:

- more expensive at run time
- after the path is calculated need joint angles in a lot of points by IK
- Discontinuity problems


## Advantages:

- near to the task specification
- advantageous for collision avoidance
- can specify the spatial shape of the path


Joint position commands

## Difficulties of trajectories in Cartesian space

1. Waypoints cannot be realized

- workspace boundaries, object collision, self-collision



## Difficulties of trajectories in Cartesian space (cont.)

2. Velocities in the vicinity of singular configurations are too high


## Difficulties of trajectories in Cartesian space (cont.)

3. Start and end configurations can be achieved, but there are different solutions

- ambiguous solutions



Joint position commands

Joint space:

- no inverse kinematics in joint space required
- the planned trajectory can be immediately applied
- no problem with singularities
- physical joint constraints can be considered


## Primitive solution

## Naive approach

Set the pose for the next time step (e.g. 10 ms later) to $B$.

- possible only in simulation
- the moving distance for a manipulator at the next time step may be too large (velocity approaches $\infty$ )


## Next best approach

- divide distance between A and B to shorter (sub-)distances
- use linear interpolation for these (sub-)distances
- respect the maximum velocity constraint


## Linear interpolation - visualization

Trajectory Generation 1 - Solutions of trajectory generation


## Problem

The physical constraints are violated

- joint velocity is limited by maximum motor rotation speed
- joint acceleration is limited by maximum motor torque

Implicitly these contraints are valid for motion in cartesian space.

- robot dynamics (joint moments resulting from the robot motion) affect the boundary condition


## Solution

- dynamical trajectory generation
- advanced optimization methods $\rightarrow$ current topic of research


## Next best approach

- Limitation of joint velocity and acceleration
- Two different methods
- trapezoidal interpolation
- polynomial interpolation


## Trapezoidal interpolation - visualization



- Position is quadratic during acceleration and deceleration, and linear elsewhere
- Linear segment with Parabolic Blends
- Velocity linearly ramps up/down to maximum velocity
- Acceleration and deceleration is constant for each trajectory segment.
- consider joint velocity and acceleration contraints
- optimal time usage (move with maximum acceleration and velocity)
- acceleration is not differentiable (the jerk is not continuous)
- start and end velocity equals 0
- not sensible for concatenating trajectories
- improved by polynomial interpolation


## Problem

Multidimensional trapezoidal interpolations

- different run time for joints (or cartesian dimensions)
- multiple velocity and acceleration contraints
- results in various time switch points
- from acceleration to continuous velocity
- from continuous velocity to deceleration
- moving along a line in joint/cartesian space is impossible.


## Trapezoidal interpolation - constraints



## Solution

- Normalization to the joint that takes longest to reach its goal
- Synchronize phase switching points and overall execution time


## Trapezoidal interpolation - normalization

Normalize to the slowest joint


- Consider velocity and acceleration boundary conditions
- calculation of extremum and duration of trajectory
- Acceleration differentiable
- continuous jerk
- smooth trajectory
- interesting only in the theory - for momentum control
- Start and end velocity may be $\neq 0$
- sensible for concatenating trajectories
- Usually a polynomial with degree of 3 (cubic spline) or 5
- Calculation of coefficient with respect to boundary constraints
- $3^{\text {rd }}$-degree polynomial: consider 4 boundary constraints
- position and velocity; start and goal
- $5^{\text {th }}$-degree polynomial: consider 6 boundary constraints
- position, velocity and acceleration; start and goal

Polynomial interpolation (cont.)


## Cubic polynomials between two configurations

- third-degree polynomial $\Rightarrow$ four constraints(position and velocity; start and goal):

$$
\begin{gathered}
\theta(t)=a_{0}+a_{1} t+a_{2} t^{2}+a_{3} t^{3} \\
\theta(t)=a_{1}+2 a_{2} t+3 a_{3} t^{2} \\
\theta \ddot{(t)}=2 a_{2}+6 a_{3} t
\end{gathered}
$$

- if the start and end velocity is 0 then

$$
\begin{align*}
\theta(0) & =\theta_{0}  \tag{36}\\
\theta\left(t_{f}\right) & =\theta_{f}  \tag{37}\\
\dot{\theta}(0) & =0  \tag{38}\\
\dot{\theta}\left(t_{f}\right) & =0 \tag{39}
\end{align*}
$$

- The solution

$$
\begin{array}{ll}
\text { eq. (36) } & a_{0}=\theta_{0} \\
\text { eq. (38) } & a_{1}=0 \\
& a_{2}=\frac{3}{t_{f}^{2}}\left(\theta_{f}-\theta_{0}\right) \\
& a_{3}=-\frac{2}{t_{f}^{3}}\left(\theta_{f}-\theta_{0}\right)
\end{array}
$$

- Similar to the previous example:
- positions of waypoints are given (same)
- velocities of waypoints are different from 0 (different)

$$
\begin{align*}
\theta(0) & =\theta_{0}  \tag{40}\\
\theta\left(t_{f}\right) & =\theta_{f}  \tag{41}\\
\dot{\theta}(0) & =\dot{\theta}_{0}  \tag{42}\\
\dot{\theta}\left(t_{f}\right) & =\dot{\theta}_{f} \tag{43}
\end{align*}
$$

- The solution

$$
\begin{aligned}
\text { eq. (40) } & a_{0} \\
\text { eq. (42) } & a_{1} \\
& =\dot{\theta}_{0} \\
a_{2} & =\frac{3}{t_{f}^{2}}\left(\theta_{f}-\theta_{0}\right)-\frac{2}{t_{f}} \dot{\theta}_{0}-\frac{1}{t_{f}} \dot{\theta}_{f} \\
a_{3} & =-\frac{2}{t_{f}^{3}}\left(\theta_{f}-\theta_{0}\right)+\frac{1}{t_{f}^{2}}\left(\dot{\theta}_{f}+\dot{\theta}_{0}\right)
\end{aligned}
$$

## Velocity calculation at the waypoints

- Manually specify waypoints
- based on cartesian linear and angle velocity of the tool frame
- Automatic calculation of waypoints in cartesian or joint space
- based on heuristics
- Automatic determination of the parameters
- based on continous acceleration at the waypoints

Example $5^{\text {th }}$-degree
$\theta(x)=a_{0}+a_{1} t+a_{2} t^{2}+a_{3} t^{3}+a_{4} t^{4}+a_{5} t^{5}$
Boundary conditions for start $\left(x=t_{0}\right)$ and goal $\left(x=t_{d}\right)$ :

- $\theta\left(t_{0}\right)=\operatorname{pos}_{\text {Start }}, \theta\left(t_{d}\right)=\operatorname{pos}_{\text {Goal }}$
- $\theta\left(\dot{t}_{0}\right)=$ vel $_{\text {Start }},\left(\dot{t}_{d}\right)=$ vel $_{\text {Goal }}$
- $\theta\left(\ddot{t}_{0}\right)=\operatorname{accstart},\left(\tilde{t}_{d}\right)=\operatorname{acc} G_{\text {Goal }}$
- The smoothest curves are generated by infinitly often differentiable functions.
- $e^{x}$
- $\sin (x), \cos (x)$
- $\log (x)($ for $x>0)$
- ...
- Polynomials are suitable for interpolation
- Problem: oscillations caused by a degree which is too high
- Piecewise polynomials with specified degree are applicable
- cubic polynomial
- splines
- B-Splines


## Factors for time optimal motion - Arc Length

If the curve in the $n$-dimensional space is given by

$$
\mathbf{q}(t)=\left[q^{1}(t), q^{2}(t), \ldots, q^{n}(t)\right]^{T}
$$

then the arc length can be defined as follows:

$$
s=\int_{0}^{t}\|\dot{\mathbf{q}}(t)\|_{2} d t
$$

where $\|\dot{\mathbf{q}}(t)\|_{2}$ is the euclidean norm of vector $d \mathbf{q}(t) / d t$ and is labeled as a flow velocity along the curve.

$$
\|\mathbf{x}\|_{2}:=\sqrt{x_{1}^{2}+\cdots+x_{n}^{2}}
$$

With the following two points given
$\mathbf{p}_{0}=\mathbf{q}\left(t_{s}\right)$ und $\mathbf{p}_{1}=\mathbf{q}\left(t_{f}\right)$,
the arc length $L$ between $\mathbf{p}_{0}$ and $\mathbf{p}_{1}$ is the integral:

$$
L=\int_{\mathbf{p}_{0}}^{\mathbf{p}_{1}} d s=\int_{t_{s}}^{t_{f}}\|\dot{\mathbf{q}}(t)\|_{2} d t
$$

"The trajectory parameters should be calculated in the way that the arc length
$L$ under the given constraints has the shortest possible value."

# Factors for time optimal motion - Curvature 

## Curvature

Defines the sharpness of a curve. A straight line has zero curvature. Curvature of large circles is smaller than of small circles.

At first the unit vector of a curve $\mathbf{q}(t)$ can be defined as

$$
\mathbf{U}=\frac{d \mathbf{q}(t)}{d s}=\frac{d \mathbf{q}(t) / d t}{d s / d t}=\frac{\dot{\mathbf{q}}(t)}{|\dot{\mathbf{q}}(t)|}
$$

If $s$ is the parameter of the arc length and $\mathbf{U}$ as the unit vector is given, the curvature of curve $\mathbf{q}(t)$ can be defined as

$$
\kappa(s)=\left|\frac{d \mathbf{U}}{d s}\right|
$$

The bending energy of a smooth curve $\mathbf{q}(t)$ over the interval $t \in[0, T]$ is defined as

$$
E=\int_{0}^{L} \kappa(s)^{2} d s=\int_{0}^{T} \kappa(t)^{2}|\dot{\mathbf{q}}(t)| d t
$$

where $\kappa(t)$ is the curvature of $\mathbf{q}(t)$.
"The bending energy $E$ of a trajectory should be as small as possible under consideration of the arc length."

## Factors for time optimal motion - Motion Time

If a motion consists of $n$ successive segments

$$
q_{j}, j \in\{1 \ldots n\}
$$

then

$$
u_{j}=t_{j+1}-t_{j}
$$

is the required time for the motion in the segment $\mathbf{q}_{j}$. The total motion time is

$$
T=\sum_{j=1}^{n-1} u_{j}
$$

- Proposed by Flash \& Hogan (1985) [7]
- Optimization Criterion minimizes the jerk in the trajectory

$$
H(x(t))=\frac{1}{2} \int_{t=t_{i}}^{t_{f}} \dddot{x}^{2} d t
$$

- The minimum-jerk solution can be written as:

$$
x(t)=x_{i}+\left(x_{i}-x_{f}\right)\left(15\left(\frac{t}{d}\right)^{4}-6\left(\frac{t}{d}\right)^{5}-10\left(\frac{t}{d}\right)^{3}\right)
$$

- Predicts bell shaped velocity profiles

$$
\dot{x}(t)=\frac{1}{d}\left(x_{i}-x_{f}\right)\left(60\left(\frac{t}{d}\right)^{3}-30\left(\frac{t}{d}\right)^{4}-30\left(\frac{t}{d}\right)^{2}\right)
$$

Minimum jerk trajectory (cont.)


## Dynamical constraints for all joints

The borders for the minimum motion time $T_{\text {min }}$ for the trajectory $\mathbf{q}_{j}^{i}(t)$ are defined over dynamical parameters of all joints.
For joint $i \in\{1 \ldots n\}$ of trajectory part $j \in\{1 \ldots m\}$ this kind of constraint can be described as follows

$$
\begin{align*}
\left|\dot{q}_{j}^{i}(t)\right| & \leq \dot{q}_{\text {max }}^{i}  \tag{44}\\
\left|\ddot{q}_{j}^{i}(t)\right| & \leq \ddot{q}_{\text {max }}^{i}  \tag{45}\\
\left|m_{j}^{i}(t)\right| & \leq m_{\text {max }}^{i} \tag{46}
\end{align*}
$$

- $m^{i}$ is the torque (moment of force) for the joint $i$ and can be calculated from the dynamical equation (motion equation).
- $\dot{q}_{\text {max }}^{i}, \ddot{q}_{\text {max }}^{i}$ and $m_{\text {max }}^{i}$ represent the important parameters of the dynamical capacity of the robot.
- Reflexxes Motion Libraries (Download, Overview)
- specialize on instantaneously generating smooth trajectories based on joint states and their limits
- Prof. Dr. Torsten Kroeger
- paper: Online Trajectory Generation: Basic Concepts for Instantaneous Reactions to Unforeseen Events [8]


## Examples of using Reflexxes in TAMS

- Real-time object shape detection using ROS, the KUKA LWR4+ and a force/torque Sensor
- to specify the target position and target velocity at the target position



## Examples of using Reflexxes in TAMS (cont.)

- Adaptive pouring of liquids based on human motions using a Robotic Arm
- to recalculate the speeds of a joint trajectory (returned by CCP) to match the original time-line of the


25

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