# Introduction to Robotics 

## Lecture 7

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Technical Aspects of Multimodal Systems

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\text { June 05, } 2020
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## Outline

## Introduction

Spatial Description and Transformations
Forward Kinematics
Robot Description
Inverse Kinematics for Manipulators
Instantaneous Kinematics
Trajectory Generation 1
Trajectory Generation 2
Dynamics
Forward and inverse Dynamics
Dynamics of Manipulators
Newton-Euler-Equation
Langrangian Equations
General dynamic equations
Robot Control

## Outline (cont.)

Task-Level planning and Motion planning
Task-Level planning and Motion planning
Architectures of Sensor-based Intelligent Systems
Summary
Conclusion and Outlook

- A multibody system is a mechanical system of single bodies
- connected by joints,
- influenced by forces
- The term dynamics describes the behavior of bodies influenced by forces
- Typical forces: weight, friction, centrifugal, magnetic, spring, ...
- kinematics just models the motion of bodies (without considering forces), therefore it can be seen as a subset of dynamics


## Forward and inverse Dynamics

We consider a force $F$ and its effect on a body:

$$
F=m \cdot a=m \cdot \dot{v}
$$

In order to solve this equation, two of the variables need to be known.

If the force $F$ and the mass of the body $m$ is known:

$$
a=\dot{v}=\frac{F}{m}
$$

Hence the following can be determined:

- velocity (by integration)
- coordinates of single bodies
- forward dynamics
- mechanical stress of bodies


## Input

$\tau_{i}=$ torque at joint $i$ that effects a trajectory $\Theta$.
$i=1, \ldots, n$, where $n$ is the number of joints.

Output
$\Theta_{i}=$ joint angle of $i$
$\dot{\Theta}_{i}=$ angular velocity of joint $i$
$\ddot{\Theta}_{i}=$ angular acceleration of joint $i$

If the time curves of the joint angles are known, it can be differentiated twice.
This way,

- internal forces
- and torques
can be obtained for each body and joint.
Problems of highly dynamic motions:
- models are not as complex as the real bodies
- differentiating twice (on sensor data) leads to high inaccuracy

Input
$\Theta_{i}=$ joint angle $i$
$\dot{\Theta}_{i}=$ angular velocity of joint $i$
$\ddot{\Theta}_{i}=$ angular acceleration of joint $i$
$i=1, \ldots, n$, where $n$ is the number of joints.

## Output

$\tau_{i}=$ required torque at joint $i$ to produce trajectory $\Theta$.

## Dynamics of Manipulators

- Forward dynamics:
- Input: joint forces / torques;
- Output: kinematics;
- Application: Simulation of a robot model.
- Inverse Dynamics:
- Input: desired trajectory of a manipulator;
- Output: required joint forces / torques;
- Application: model-based control of a robot.

$$
\begin{aligned}
\tau(t) & \rightarrow \text { direct dynamics } \rightarrow \mathbf{q}(t),(\dot{\mathbf{q}}(t), \ddot{\mathbf{q}}(t)) \\
\mathbf{q}(t) & \rightarrow \text { inverse dynamics } \rightarrow \tau(t)
\end{aligned}
$$

Unlike kinematics, the inverse dynamics is easier to solve than forward dynamics

Two methods for calculation:

- Analytical methods
- based on Lagrangian equations
- Synthetic methods:
- based on the Newton-Euler equations


## Computation time

Complexity of solving the Lagrange-Euler-model is $O\left(n^{4}\right)$ where $n$ is the number of joints.
$n=6: 66,271$ multiplications and 51,548 additions.

The description of manipulator dynamics is directly based on the relations between the kinetic $K$ and potential energy $P$ of the manipulator joints.

Here:

- constraining forces are not considered
- deep knowledge of mechanics is necessary
- high effort of defining equations
- can be solved by software

The Lagrangian function $L$ is defined as the difference between kinetic energy $K$ and potential energy $P$ of the system.

$$
L\left(q_{i}, \dot{q}_{i}\right)=K\left(q_{i}, \dot{q}_{i}\right)-P\left(q_{i}\right)
$$

- K: kinetic energy due to linear velocity of the link's center of mass and angular velocity of the link
- $P$ : potential energy stored in the manipulator that is the sum of the potential energy in the individual links

The Lagrangian function $L$ is defined as:

$$
L\left(q_{i}, \dot{q}_{i}\right)=K\left(q_{i}, \dot{q}_{i}\right)-P\left(q_{i}\right)
$$

## Theorem

The motion equations of a mechanical system with coordinates $\mathbf{q} \in \Theta^{n}$ and the Lagrangian function $L$ is defined by:

$$
\frac{d}{d t} \frac{\partial L}{\partial \dot{q}_{i}}-\frac{\partial L}{\partial q_{i}}=F_{i}, \quad i=1, \ldots, n
$$

where
$q_{i}$ : the coordinates, where the kinetic and potential energy is defined;
$\dot{q}_{i}$ : the velocity;
$F_{i}$ : the force or torque, depending on the type of joint (rotational or linear)

- Determine the kinematics from the fixed base to the TCP (relative kinematics)
- The resulting acceleration leads to forces towards rigid bodies
- The combination of constraining forces, payload forces, weight forces and working forces can be defined for every rigid body. All torques and momentums need to be in balance
- Solving this formula leads to the joint forces
- Especially suitable for serial kinematics of manipulator


## Recursive Newton-Euler Method (cont.)

1. Newton's equation

$$
F=m \dot{v}_{c}
$$

where $F$ is the force acting at the center of mass of a body, $m$ is the total mass of the body, $v_{c}$ is the acceleration.

2. Euler's equation

$$
\tau={ }^{C} \mathbf{l} \dot{\omega}+\omega \times{ }^{C} \mathbf{l} \omega
$$



- where ${ }^{C} \mathbf{I}$ is the inertia tensor of the body written in a frame $C$, whose origin is located at the center of the mass.

$$
C_{I}=\left[\begin{array}{ccc}
I_{x x} & -I_{x y} & -I_{x z} \\
-I_{x y} & I_{y y} & -I_{y z} \\
-I_{x z} & -I_{y z} & 1 z z
\end{array}\right]
$$

- $\tau$ is the torque
- $\omega, \dot{\omega}$ are the angular velocity and angular acceleration respectively
- Functional affordance
- trajectory and velocity of links
- load on a link
- Control quantity
- velocity and acceleration of joints
- forces and torques
- Robot-specific elements
- geometry
- mass distribution
- Determining joint forces and torques for one point of a trajectory $(\Theta, \dot{\Theta}, \ddot{\Theta})$
- Determining the motion of a link or the complete manipulator for given joint-forces and -torques ( $\tau$ )
To achieve this the mathematical model is applied.


## Formulation of robot dynamics

- Combining the different influence factors in the robot specific motion equation from kinematics $(\Theta, \dot{\Theta}, \ddot{\Theta})$
- Practically the Newton-, Euler- and motion-equation for each joint are combined
- Advantages: numerically efficient, applicable for complex geometry, can be modularized
- We can determine the forces with the Newton-equation
- The Euler-equation provides the torque
- The combination provides force and torque for each joint.


## Example: A 2 DOF manipulator

Dynamics of a multibody system, example: a two joint manipulator.


Using Newton's second law, the forces at the center of mass at link 1 and 2 are:

$$
\mathbf{F}_{1}=m_{1} \ddot{\mathbf{r}}_{1}
$$

$$
\mathbf{F}_{2}=m_{2} \ddot{\mathbf{r}}_{2}
$$

where

$$
\begin{gathered}
\mathbf{r}_{1}=\frac{1}{2} l_{1}\left(\cos \theta_{1} \vec{i}+\sin \theta_{1} \vec{j}\right) \\
\mathbf{r}_{2}=2 \mathbf{r}_{1}+\frac{1}{2} l_{2}\left[\cos \left(\theta_{1}+\theta_{2}\right) \vec{i}+\sin \left(\theta_{1}+\theta_{2}\right) \vec{j}\right]
\end{gathered}
$$

Euler equations:

$$
\begin{aligned}
& \tau_{1}=\mathbf{I}_{1} \dot{\omega}_{1}+\omega_{1} \times \mathbf{I}_{1} \omega_{1} \\
& \tau_{2}=\mathbf{I}_{2} \dot{\omega}_{2}+\omega_{2} \times \mathbf{I}_{2} \omega_{2}
\end{aligned}
$$

where

$$
\begin{aligned}
& \mathbf{I}_{1}=\frac{m_{1} /_{1}^{2}}{12}+\frac{m_{1} R^{2}}{4} \\
& \mathbf{I}_{2}=\frac{m_{2} /_{2}^{2}}{12}+\frac{m_{2} R^{2}}{4}
\end{aligned}
$$

## Newton-Euler-Equations for 2 DOF manipulator (cont.)

The angular velocities and angular accelerations are:

$$
\begin{gathered}
\omega_{1}=\dot{\theta}_{1} \\
\omega_{2}=\dot{\theta}_{1}+\dot{\theta}_{2} \\
\dot{\omega}_{1}=\ddot{\theta}_{1} \\
\dot{\omega}_{2}=\ddot{\theta}_{1}+\ddot{\theta}_{2}
\end{gathered}
$$

As $\omega_{i} \times \mathbf{I}_{i} \omega_{i}=0$, the torques at the center of mass of links 1 and 2 are:

$$
\begin{gathered}
\tau_{1}=\mathbf{l}_{1} \ddot{\theta}_{1} \\
\tau_{2}=\mathbf{I}_{2}\left(\ddot{\theta}_{1}+\ddot{\theta}_{2}\right)
\end{gathered}
$$

$\mathbf{F}_{1}, \mathbf{F}_{2}, \tau_{1}, \tau_{2}$ are used for force and torque balance and are solved for joint 1 and 2.

## Example: A two joint manipulator



The kinetic energy of mass $m_{1}$ is:

$$
K_{1}=\frac{1}{2} m_{1} d_{1}^{2}{\dot{\theta_{1}}}^{2}
$$

The potential energy is:

$$
P_{1}=-m_{1} g d_{1} \cos \left(\theta_{1}\right)
$$

The cartesian positions are:

$$
\begin{gathered}
x_{2}=d_{1} \sin \left(\theta_{1}\right)+d_{2} \sin \left(\theta_{1}+\theta_{2}\right) \\
y_{2}=-d_{1} \cos \left(\theta_{1}\right)-d_{2} \cos \left(\theta_{1}+\theta_{2}\right)
\end{gathered}
$$

The cartesian components of velocity are:

$$
\begin{aligned}
& \dot{x}_{2}=d_{1} \cos \left(\theta_{1}\right) \dot{\theta}_{1}+d_{2} \cos \left(\theta_{1}+\theta_{2}\right)\left(\dot{\theta}_{1}+\dot{\theta}_{2}\right) \\
& \dot{y}_{2}=d_{1} \sin \left(\theta_{1}\right) \dot{\theta}_{1}+d_{2} \sin \left(\theta_{1}+\theta_{2}\right)\left(\dot{\theta}_{1}+\dot{\theta}_{2}\right)
\end{aligned}
$$

The square of velocity is:

$$
v_{2}^{2}={\dot{x_{2}}}^{2}+{\dot{y_{2}}}^{2}
$$

The kinetic energy of link 2 is:

$$
K_{2}=\frac{1}{2} m_{2} v_{2}^{2}
$$

The potential energy of link 2 is:

$$
P_{2}=-m_{2} g d_{1} \cos \left(\theta_{1}\right)-m_{2} g d_{2} \cos \left(\theta_{1}+\theta_{2}\right)
$$

The Lagrangian function is:

$$
L=\left(K_{1}+K_{2}\right)-\left(P_{1}+P_{2}\right)
$$

The force/torque to joint 1 and 2 are:

$$
\begin{aligned}
& \tau_{1}=\frac{d}{d t} \frac{\partial L}{\partial \dot{\theta}_{1}}-\frac{\partial L}{\partial \theta_{1}} \\
& \tau_{2}=\frac{d}{d t} \frac{\partial L}{\partial \dot{\theta}_{2}}-\frac{\partial L}{\partial \theta_{2}}
\end{aligned}
$$

## Langragian Method for two joint manipulator (cont.)

$\tau_{1}$ and $\tau_{2}$ are expressed as follows:

$$
\begin{aligned}
\tau_{1}= & D_{11} \ddot{\theta}_{1}+D_{12} \ddot{\theta}_{2}+D_{111} \dot{\theta}_{1}^{2}+D_{122} \dot{\theta}_{2}^{2} \\
& +D_{112} \dot{\theta}_{1} \dot{\theta}_{2}+D_{121} \dot{\theta}_{2} \dot{\theta}_{1}+D_{1} \\
\tau_{2}= & D_{21} \ddot{\theta}_{1}+D_{22} \ddot{\theta}_{2}+D_{211} \dot{\theta}_{1}^{2}+D_{222} \dot{\theta}_{2}^{2} \\
& +D_{212} \dot{\theta}_{1} \dot{\theta}_{2}+D_{221} \dot{\theta}_{2} \dot{\theta}_{1}+D_{2}
\end{aligned}
$$

where
$D_{i i}$ : the inertia to joint $i$;
$D_{i j}$ : the coupling of inertia between joint $i$ and $j$;
$D_{i j j}$ : the coefficients of the centripetal force to joint $i$ because of the velocity of joint $j$;
$D_{i i k}\left(D_{i k i}\right)$ : the coefficients of the Coriolis force to joint $i$ effected by the velocities of joint $i$ and $k$;
$D_{i}$ : the gravity of joint $i$.

## General dynamic equations of a manipulator

$$
\tau=M(\Theta) \ddot{\Theta}+V(\Theta, \dot{\Theta})+G(\Theta)
$$

$M(\Theta)$ : the position dependent $n \times n$-mass matrix of a manipulator For the example given above:

$$
M(\Theta)=\left[\begin{array}{ll}
D_{11} & D_{12} \\
D_{21} & D_{22}
\end{array}\right]
$$

$V(\Theta, \dot{\Theta})$ : an $n \times 1$-vector of centripetal and coriolis coefficients For the example given above:

$$
V(\Theta, \dot{\Theta})=\left[\begin{array}{l}
D_{111} \dot{\theta}_{1}^{2}+D_{122} \dot{\theta}_{2}^{2}+D_{112} \dot{\theta}_{1} \dot{\theta}_{2}+D_{121} \dot{\theta}_{2} \dot{\theta}_{1} \\
D_{211} \dot{\theta}_{1}^{2}+D_{222} \dot{\theta}_{2}^{2}+D_{212} \dot{\theta}_{1} \dot{\theta}_{2}+D_{221} \dot{\theta}_{2} \dot{\theta}_{1}
\end{array}\right]
$$

- a term such as $D_{111} \dot{\theta}_{1}^{2}$ is caused by coriolis force;
- a term such as $D_{112} \dot{\theta}_{1} \dot{\theta}_{2}$ is caused by coriolis force and depends on the (math.) product of the two velocities.
- $G(\Theta)$ : a term of velocity, depends on $\Theta$.
- for the example given above

$$
G(\Theta)=\left[\begin{array}{l}
D_{1} \\
D_{2}
\end{array}\right]
$$

## Robot dynamics with flexible joint model

$$
\begin{aligned}
M(q) \ddot{q}+C(q, \dot{q}) \dot{q}+g(q) & =\tau+D K^{-1} \dot{\tau}+\tau_{e x t} \\
B \ddot{\theta}+\tau+D K^{-1} \dot{\tau} & =\tau_{m}-\tau_{f} \\
\tau & =K(\theta-q)
\end{aligned}
$$

- flexible joint as a two-mass model



## Applications of robot dynamics

KUKA LWR's model-based control

- shortening the motion time without generating overshoots
- giving large reduction of the tracking error



## Applications of robot dynamics (cont.)

KUKA iiwa's hand teaching

- Free movement by hand with dynamics compensation on each joint



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