



Universität Hamburg

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Department of Informatics



Introduction to Robotics

Lecture 6

Lasse Einig, Jianwei Zhang

[einig, zhang]@informatik.uni-hamburg.de



University of Hamburg
Faculty of Mathematics, Informatics and Natural Sciences
Department of Informatics

Technical Aspects of Multimodal Systems

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Introduction

Coordinate systems

Kinematic Equations

Robot Description

Inverse Kinematics for Manipulators

Differential motion with homogeneous transformations

Jacobian

Trajectory planning

- Trajectory generation

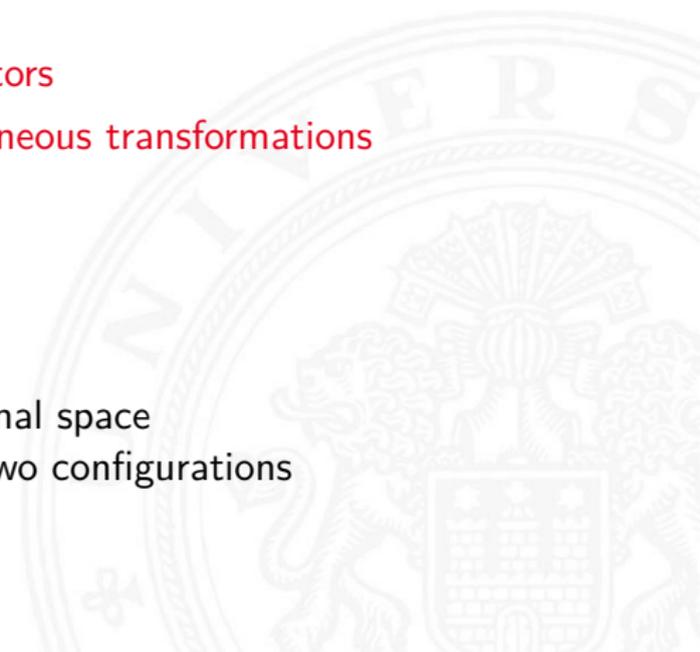
- Generation of trajectories

- Trajectories in multidimensional space

- Cubic polynomials between two configurations

- Optimizing motion

Trajectory generation





Outline (cont.)

Trajectory planning

Introduction to Robotics

Dynamics

Principles of Walking

Robot Control

Task-Level Programming and Trajectory Generation

Task-level Programming and Path Planning

Task-level Programming and Path Planning

Architectures of Sensor-based Intelligent Systems

Summary

Conclusion and Outlook





Definition

A trajectory is a time history of

position,
velocity and
acceleration

for each DOF

Describes motion of TCP frame relative to base frame

- ▶ abstract from joint configuration

Series of discrete poses (TCP or joint configuration)

- ▶ usually fixed temporal intervals
- ▶ possibly fixed distances, key frames



Problem

I am at point A and want move to point B.

- ▶ How do I get to point B?
- ▶ How long does it take me to get to point B?
- ▶ Which constraints exist for moving from A to B?

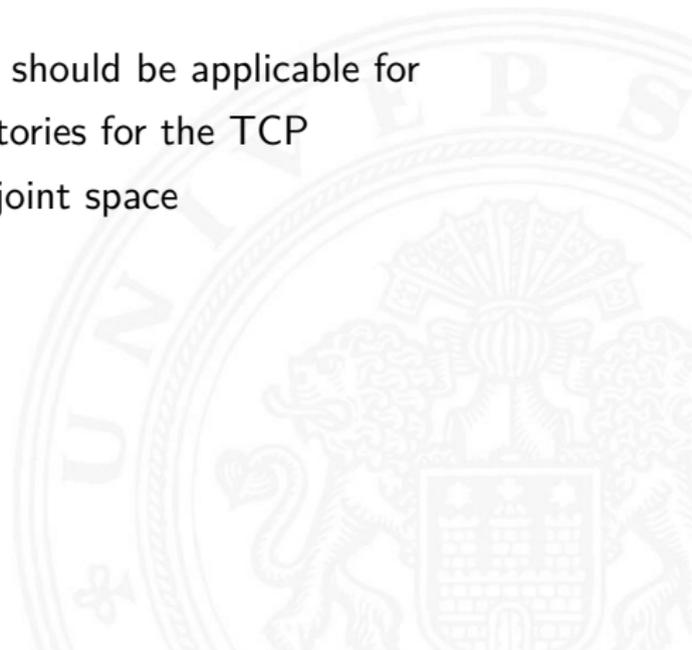
Solution

- ▶ generate a possible trajectory
- ▶ trajectory planning
- ▶ describe intermediate poses (waypoints)



The methods for path generation should be applicable for

- ▶ calculation of cartesian trajectories for the TCP
- ▶ calculation for trajectories in joint space





Naive approach

Set the pose for the next time step (e.g. 10 ms later) to B.

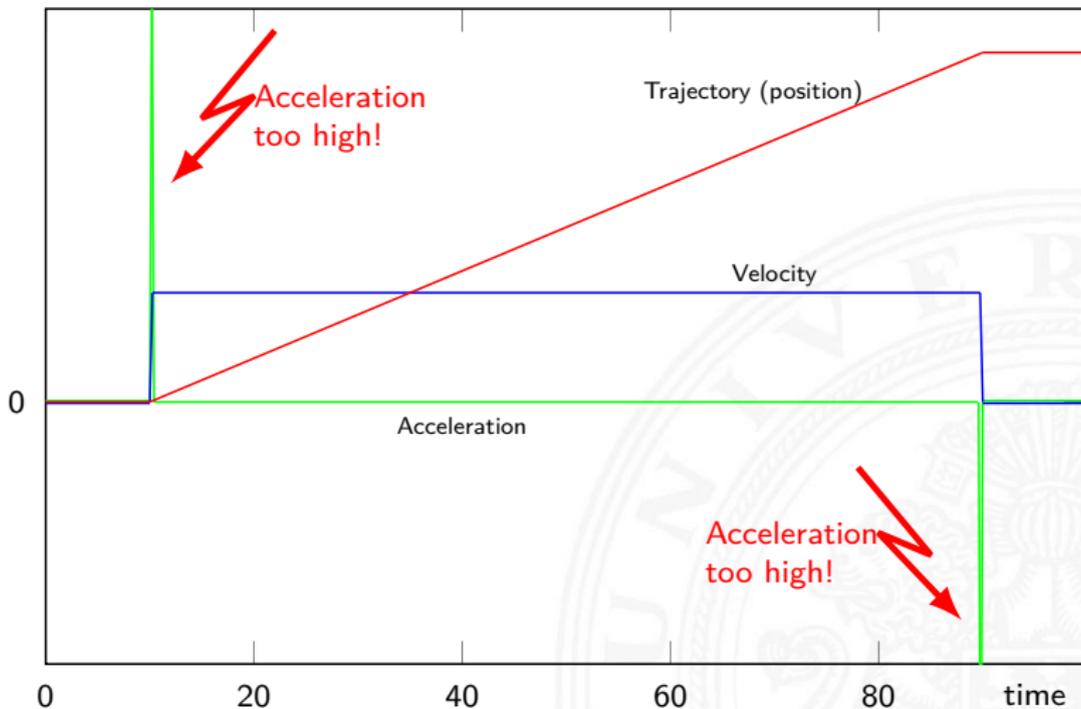
- ▶ possible only in simulation
- ▶ the moving distance for a manipulator at the next time step may be too large (velocity approaches ∞)



Next best approach

- ▶ divide distance between A and B to shorter (sub-)distances
- ▶ use linear interpolation for these (sub-)distances
- ▶ respect the maximum velocity constraint

Linear interpolation – visualization



Problem

The physical constraints are violated

- ▶ joint velocity is limited by maximum motor rotation speed
- ▶ joint acceleration is limited by maximum motor torque

Implicitly these constraints are valid for motion in cartesian space.

- ▶ robot dynamics (joint moments resulting from the robot motion) affect the boundary condition

Solution

- ▶ dynamical trajectory planning
- ▶ advanced optimization methods → current topic of research

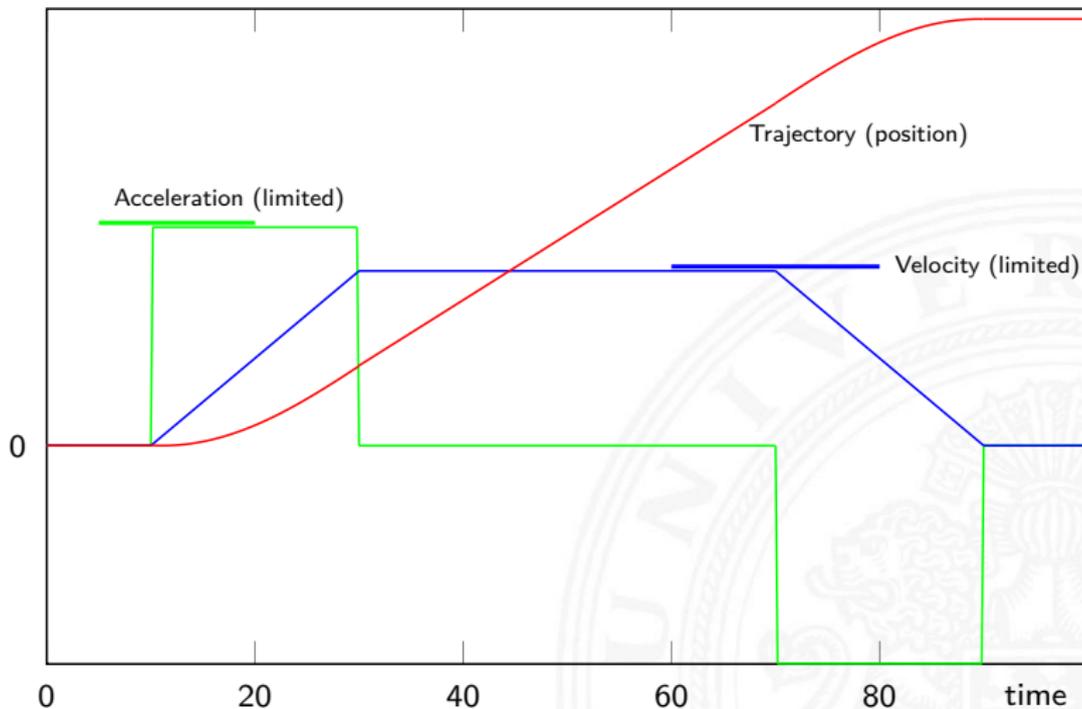


Next best approach

- ▶ Limitation of joint velocity and acceleration
- ▶ Two different methods
 - ▶ trapezoidal interpolation
 - ▶ polynomial interpolation



Trapezoidal interpolation – visualization





- ▶ consider joint velocity and acceleration constraints
- ▶ optimal time usage (move with maximum acceleration and velocity)
- ▶ acceleration is not differentiable (the jerk is not continuous)
- ▶ start and end velocity equals 0
 - ▶ not sensible for concatenating trajectories
 - ▶ improved by polynomial interpolation



Problem

Multidimensional trapezoidal interpolations

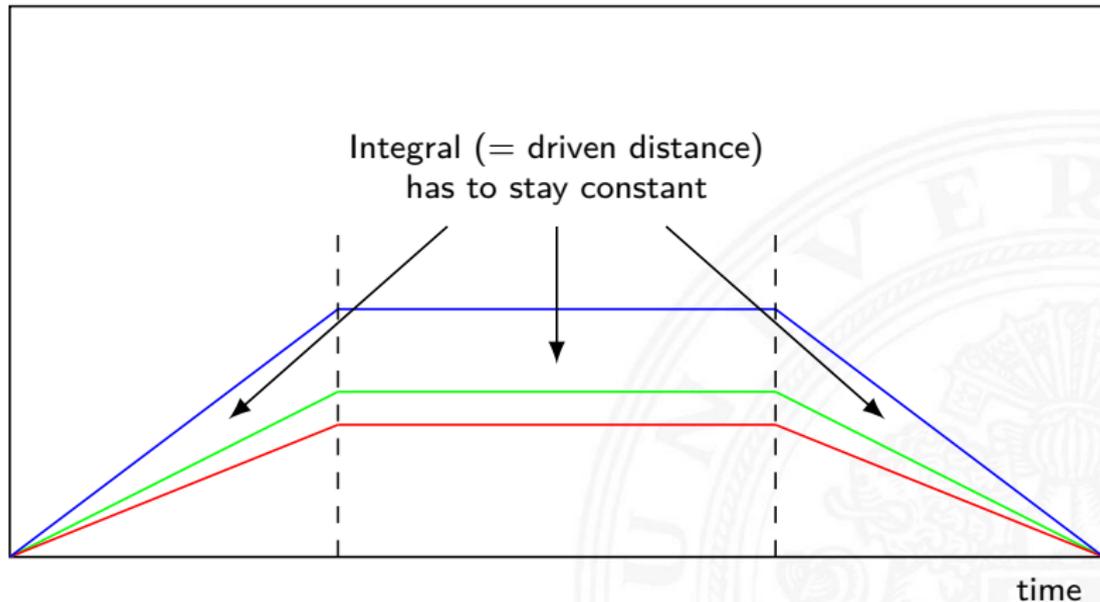
- ▶ different run time for joints (or cartesian dimensions)
- ▶ multiple velocity and acceleration constraints
- ▶ results in various time switch points
 - ▶ from acceleration to continuous velocity
 - ▶ from continuous velocity to deceleration
 - ▶ moving along a line in joint/cartesian space is impossible.

Solution

- ▶ Normalization to the slowest joint
- ▶ Use jerk and arrival time of the slowest joint instead of velocity.

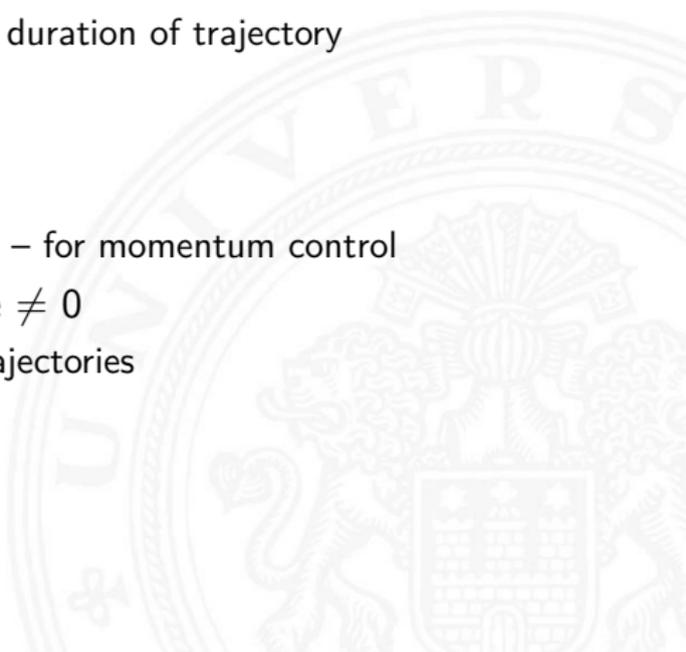
Trapezoidal interpolation – normalization (cont.)

Normalize to the slowest joint





- ▶ Consider velocity and acceleration boundary conditions
 - ▶ calculation of extremum and duration of trajectory
- ▶ Acceleration differentiable
 - ▶ continuous jerk
 - ▶ smooth trajectory
 - ▶ interesting only in the theory – for momentum control
- ▶ Start and end velocity may be $\neq 0$
 - ▶ sensible for concatenating trajectories





Polynomial interpolation (cont.)

- ▶ Usually a polynomial with degree of 3 (cubic spline) or 5
- ▶ Calculation of coefficient with respect to boundary constraints
 - ▶ 3^{rd} -degree polynomial: consider 4 boundary constraints
 - ▶ position and velocity; start and goal
 - ▶ 5^{th} -degree polynomial: consider 6 boundary constraints
 - ▶ position, velocity and acceleration; start and goal

Example 5th-degree

$$f(x) = a_0 + a_1x + a_2x^2 + a_3x^3 + a_4x^4 + a_5x^5$$

Boundary conditions for start ($x = t_0$) and goal ($x = t_d$):

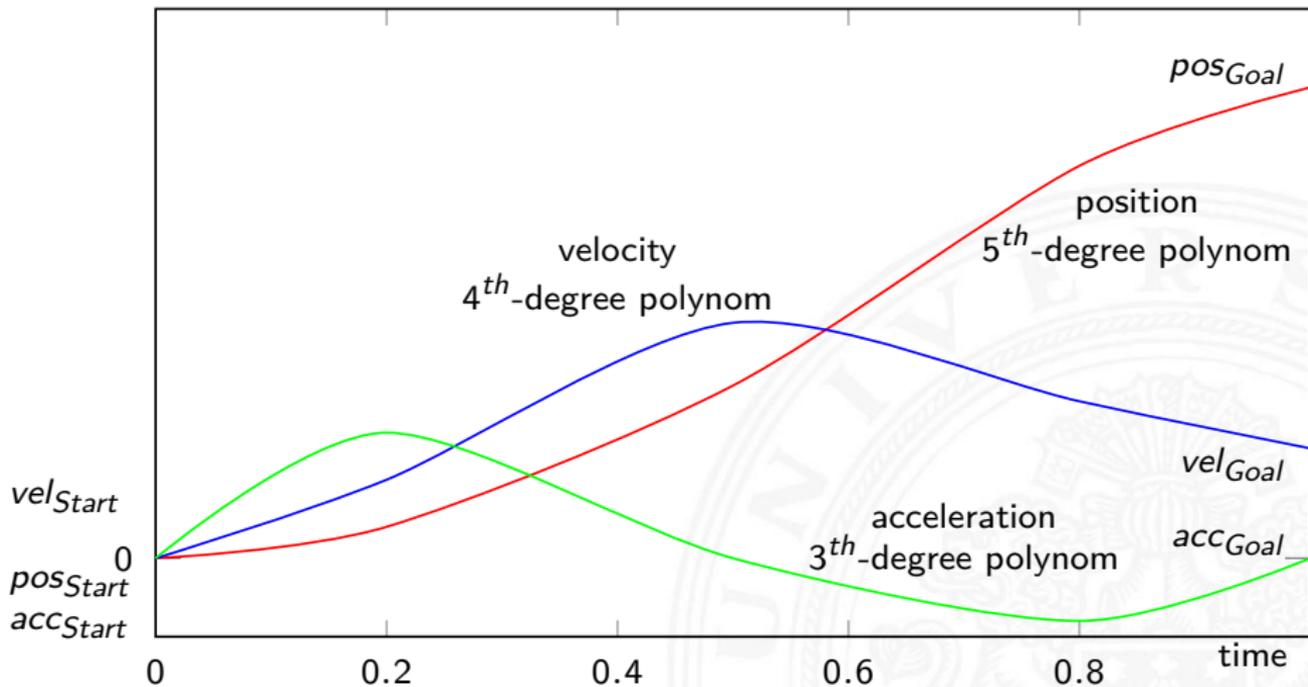
- ▶ $f(t_0) = pos_{Start}, f(t_d) = pos_{Goal}$
- ▶ $f'(t_0) = vel_{Start}, f'(t_d) = vel_{Goal}$
- ▶ $f''(t_0) = acc_{Start}, f''(t_d) = acc_{Goal}$

t : formal time from the interval $[0;1]$

Proper position interpolation from start (A) to goal (B)

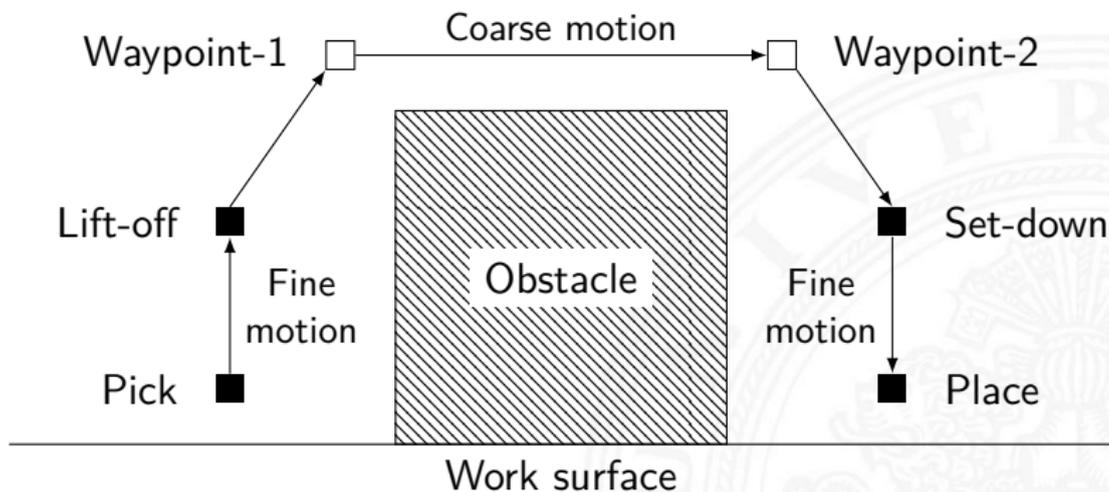
$$P(t) = Af(t) + Bf(1 - t)$$

Polynomial interpolation (cont.)



Boundary constraints

Pick-and-Place example





Boundary constraints (cont.)

Pick-and-Place example

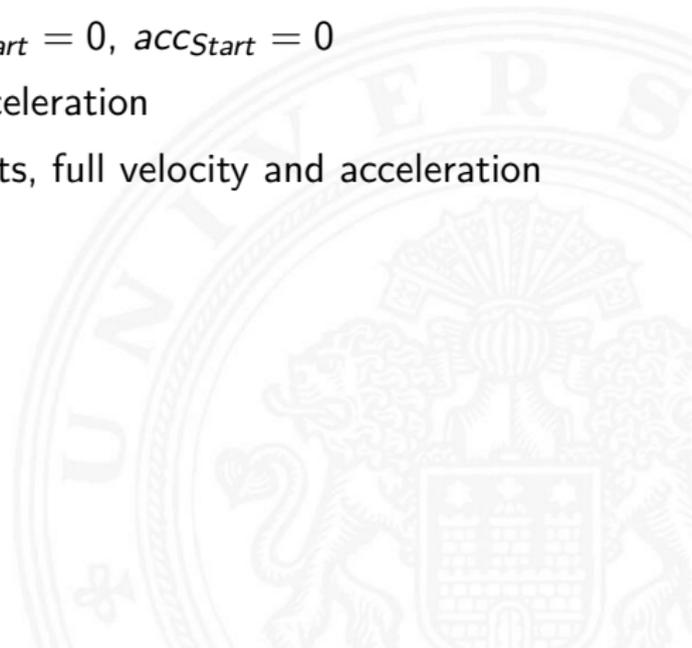
Pick $pos_{start} = object, vel_{start} = 0, acc_{start} = 0$

Lift-off limited velocity and acceleration

Motion continuous via waypoints, full velocity and acceleration

Set-down similar to Lift-off

Place similar to Pick



Task

- ▶ find trajectory for moving the robot from start to goal pose
 - ▶ calculate
 - ▶ interpolate
 - ▶ approximate
- ▶ use continuous functions of time

Solution:

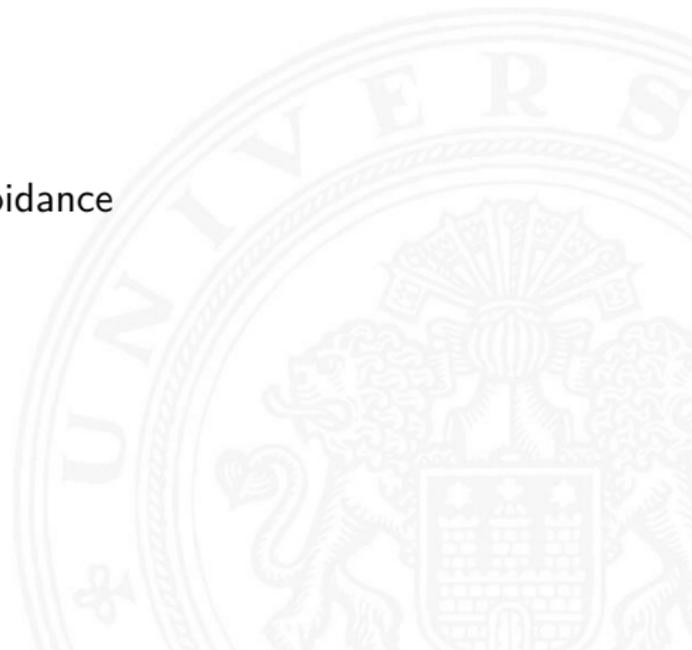
- ▶ Cartesian space
- ▶ Joint Space



Generation of trajectories (cont.)

Cartesian space:

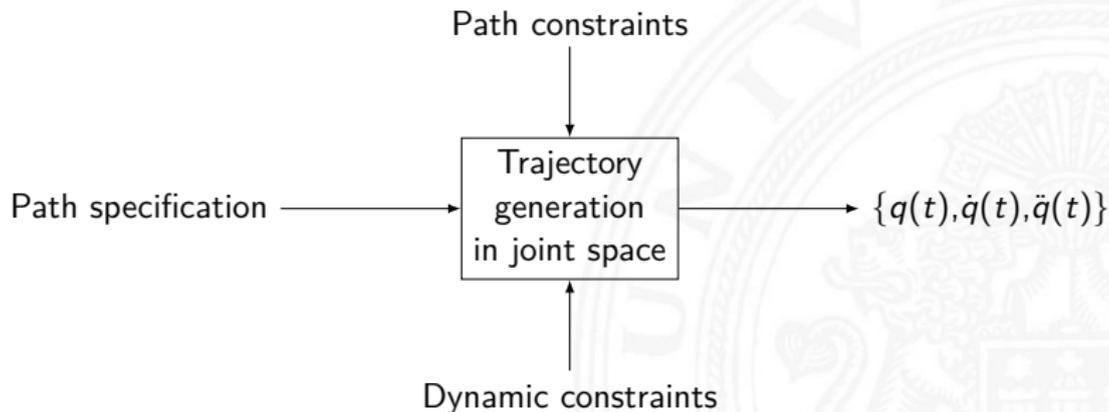
- ▶ near to the task specification
- ▶ advantageous for collision avoidance



Generation of trajectories (cont.)

Joint space:

- ▶ no inverse kinematics in joint space required
- ▶ the planned trajectory can be immediately applied
- ▶ physical joint constraints can be considered





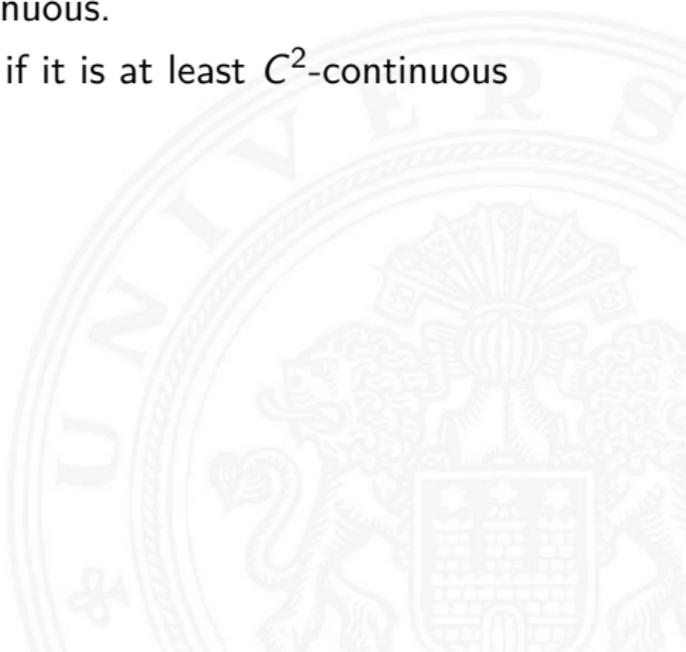
Trajectories in multidimensional space

- ▶ Changes in position, velocity and acceleration of all joints are analyzed over a period of time
- ▶ Trajectory with n DOF is a parameterized function $q(t)$ with values in its motion region.
- ▶ Trajectory $q(t)$ of a robot with n DOF is then a vector of n parameterized functions $q_i(t), i \in \{1 \dots n\}$ with one common parameter t :

$$q(t) = [q_1(t), q_2(t), \dots, q_n(t)]^T$$



- ▶ A trajectory is C^k -continuous, if all derivatives up to the k -th (including) exist and are continuous.
- ▶ A trajectory is called *smooth*, if it is at least C^2 -continuous
- ▶ $q(x)$ is the trajectory,
- ▶ $\dot{q}(x)$ is the velocity,
- ▶ $\ddot{q}(x)$ is the acceleration,
- ▶ $\dddot{q}(x)$ is the jerk



Remarks on generation of trajectories

- ▶ The smoothest curves are generated by infinitely often differentiable functions.
 - ▶ e^x
 - ▶ $\sin(x)$, $\cos(x)$
 - ▶ $\log(x)$ (for $x > 0$)
 - ▶ ...
- ▶ Polynomials are suitable for interpolation
 - ▶ Problem: oscillations caused by a degree which is too high
- ▶ Piecewise polynomials with specified degree are applicable
 - ▶ cubic polynomial
 - ▶ splines
 - ▶ B-Splines
 - ▶ ...



Cubic polynomials between two configurations

- ▶ third-degree polynomial \Rightarrow four constraints:

$$\theta(t) = a_0 + a_1t + a_2t^2 + a_3t^3$$

- ▶ if the start and end velocity is 0 then

$$\theta(0) = \theta_0 \tag{70}$$

$$\theta(t_f) = \theta_f \tag{71}$$

$$\dot{\theta}(0) = 0 \tag{72}$$

$$\dot{\theta}(t_f) = 0 \tag{73}$$

Cubic polynomials between two configurations (cont.)

► The solution

$$\text{eq. (70)} \quad a_0 = \theta_0$$

$$\text{eq. (72)} \quad a_1 = 0$$

$$a_2 = \frac{3}{t_f^2}(\theta_f - \theta_0)$$

$$a_3 = -\frac{2}{t_f^3}(\theta_f - \theta_0)$$

Cubic polynomials with waypoints and velocities

- ▶ Similar to the previous example:
 - ▶ positions of waypoints are given (same)
 - ▶ velocities of waypoints are different from 0 (different)

$$\theta(0) = \theta_0 \quad (74)$$

$$\theta(t_f) = \theta_f \quad (75)$$

$$\dot{\theta}(0) = \dot{\theta}_0 \quad (76)$$

$$\dot{\theta}(t_f) = \dot{\theta}_f \quad (77)$$

Cubic polynomials with waypoints and velocities (cont.)

► The solution

$$\text{eq. (74)} \quad a_0 = \theta_0$$

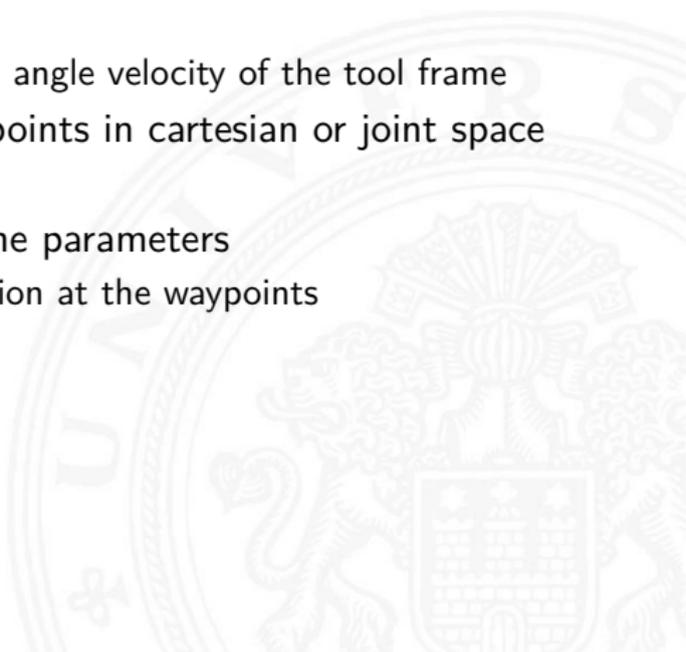
$$\text{eq. (76)} \quad a_1 = \dot{\theta}_0$$

$$a_2 = \frac{3}{t_f^2}(\theta_f - \theta_0) - \frac{2}{t_f}\dot{\theta}_0 - \frac{1}{t_f}\dot{\theta}_f$$

$$a_3 = -\frac{2}{t_f^3}(\theta_f - \theta_0) + \frac{1}{t_f^2}(\dot{\theta}_f + \dot{\theta}_0)$$



- ▶ Manually specify waypoints
 - ▶ based on cartesian linear and angle velocity of the tool frame
- ▶ Automatic calculation of waypoints in cartesian or joint space
 - ▶ based on heuristics
- ▶ Automatic determination of the parameters
 - ▶ based on continuous acceleration at the waypoints



Factors for time optimal motion – Arc Length

If the curve in the n -dimensional K space is given by

$$\mathbf{q}(t) = [q^1(t), q^2(t), \dots, q^n(t)]^T$$

then the **arc length** can be defined as follows:

$$s = \int_0^t \|\dot{\mathbf{q}}(t)\|_2 dt$$

where $\|\dot{\mathbf{q}}(t)\|_2$ is the euclidean norm of vector $d\mathbf{q}(t)/dt$ and is labeled as a flow velocity along the curve.

$$\|\mathbf{x}\|_2 := \sqrt{x_1^2 + \dots + x_n^2}$$



Factors for time optimal motion – Arc Length (cont.)

With the following two points given

$$\mathbf{p}_0 = \mathbf{q}(t_s) \text{ und } \mathbf{p}_1 = \mathbf{q}(t_f),$$

the arc length L between \mathbf{p}_0 and \mathbf{p}_1 is the integral:

$$L = \int_{\mathbf{p}_1}^{\mathbf{p}_0} ds = \int_{t_s}^{t_f} \|\dot{\mathbf{q}}(t)\|_2 dt$$

“The trajectory parameters should be calculated in the way that the arc length L under the given constraints has the shortest possible value.”

Factors for time optimal motion – Arc Length (cont.)

- ▶ trajectory of circle

$$q(t) = c(t) = [r \cos(t), r \sin(t)]^T$$

- ▶ arc length L of circle (circumference)

$$L = \int_0^{2\pi} \|\dot{c}(t)\|_2 dt \quad (78)$$

$$= \int_0^{2\pi} \left\| \begin{bmatrix} -r \sin(t) \\ r \cos(t) \end{bmatrix} \right\|_2 dt \quad (79)$$

$$= \int_0^{2\pi} \sqrt{r^2(\sin^2(t) + \cos^2(t))} dt \quad (80)$$

$$= \int_0^{2\pi} r dt \quad (81)$$

$$L = 2\pi r \quad (82)$$

Curvature

Defines the sharpness of a curve. A straight line has zero curvature. Curvature of large circles is smaller than of small circles.

At first the *unit vector* of a curve $\mathbf{q}(t)$ can be defined as

$$\mathbf{U} = \frac{d\mathbf{q}(t)}{ds} = \frac{d\mathbf{q}(t)/dt}{ds/dt} = \frac{\dot{\mathbf{q}}(t)}{|\dot{\mathbf{q}}(t)|}$$

If s is the parameter of the *arc length* and \mathbf{U} as the *unit vector* is given, the **curvature** of curve $\mathbf{q}(t)$ can be defined as

$$\kappa(s) = \left| \frac{d\mathbf{U}}{ds} \right|$$

Factors for time optimal motion – Curvature (cont.)

$$\text{with } \kappa(s) = \left| \frac{d\mathbf{U}}{ds} \right| \rightarrow \text{curvature}$$

If the parameter t , the first derivative $\dot{\mathbf{q}} = d\mathbf{q}(t)/dt$ and the second derivative $\ddot{\mathbf{q}} = d\dot{\mathbf{q}}(t)/dt$ for the curve $\mathbf{q}(t)$ are given, then the *curvature* can be calculated from the following representation

$$\kappa(t) = \frac{|\dot{\mathbf{q}} \times \ddot{\mathbf{q}}|}{|\dot{\mathbf{q}}|^3} = \frac{(\dot{\mathbf{q}}^2 \cdot \ddot{\mathbf{q}}^2 - (\dot{\mathbf{q}} \cdot \ddot{\mathbf{q}})^2)^{1/2}}{|\dot{\mathbf{q}}|^3}$$

where $\dot{\mathbf{q}} \times \ddot{\mathbf{q}}$ is the cross product and $\dot{\mathbf{q}} \cdot \ddot{\mathbf{q}}$ is the dot product

Factors for time optimal motion – Curvature (cont.)

with $q(t) = c(t) = [r \cos(t), r \sin(t)]^T \rightarrow$ trajectory of a circle

$$\dot{c}(t) = [-r \sin(t), r \cos(t)]^T$$

$$\ddot{c}(t) = [-r \cos(t), -r \sin(t)]^T$$

$$\dot{c}^2(t) = r^2 \sin^2(t) + r^2 \cos^2(t) = r^2$$

$$\ddot{c}^2(t) = r^2 \cos^2(t) + r^2 \sin^2(t) = r^2$$

$$\dot{c}(t) \cdot \ddot{c}(t) = r^2 \sin(t) \cos(t) - r^2 \cos(t) \sin(t) = 0$$

Curvature of a circle

$$\kappa(t) = \frac{(\dot{c}^2 \cdot \ddot{c}^2 - (\dot{c} \cdot \ddot{c})^2)^{1/2}}{|\dot{c}|^3} = \frac{\sqrt{r^4}}{r^3} = \frac{1}{r}$$

Factors for time optimal motion – Bending Energy

The **bending energy** of a smooth curve $\mathbf{q}(t)$ over the interval $t \in [0, T]$ is defined as

$$E = \int_0^L \kappa(s)^2 ds = \int_0^T \kappa(t)^2 |\dot{\mathbf{q}}(t)| dt$$

where $\kappa(t)$ is the curvature of $\mathbf{q}(t)$.

“The bending energy E of a trajectory should be as small as possible under consideration of the arc length.”

Factors for time optimal motion – Motion Time

If a motion consists of n successive segments

$$q_j, j \in \{1 \dots n\}$$

then

$$u_j = t_{j+1} - t_j$$

is the required time for the motion in the segment q_j . The total motion time is

$$T = \sum_{j=1}^{n-1} u_j$$

The borders for the minimum motion time T_{min} for the trajectory $\mathbf{q}_j^i(t)$ are defined over dynamical parameters of all joints.

For joint $i \in \{1 \dots n\}$ of trajectory part $j \in \{1 \dots m\}$ this kind of constraint can be described as follows

$$|\dot{q}_j^i(t)| \leq \dot{q}_{max}^i \quad (83)$$

$$|\ddot{q}_j^i(t)| \leq \ddot{q}_{max}^i \quad (84)$$

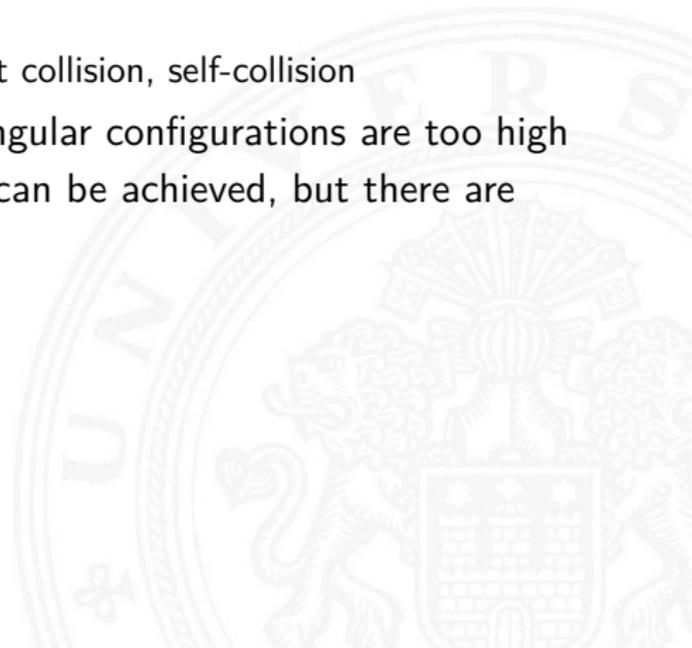
$$|m_j^i(t)| \leq m_{max}^i \quad (85)$$

- ▶ m^i is the torque (moment of force) for the joint i and can be calculated from the dynamical equation (motion equation).
- ▶ \dot{q}_{max}^i , \ddot{q}_{max}^i and m_{max}^i represent the important parameters of the dynamical capacity of the robot.



Difficulties for cartesian space trajectory generation

- ▶ Waypoints cannot be realized
 - ▶ workspace boundaries, object collision, self-collision
- ▶ Velocities in the vicinity of singular configurations are too high
- ▶ Start and end configurations can be achieved, but there are different solutions
 - ▶ ambiguous solutions



- ▶ The following algorithm should create the smallest set of waypoints in the joint space under a predefined deviation $\epsilon > 0$.
- ▶ Therefore the deviation between the trajectory $\mathbf{q}(t)$ and the given line $\langle \mathbf{w}_0, \mathbf{w}_1 \rangle$ must be smaller than ϵ .

Algorithm(Bounded_Deviation)

1. Calculation of possible configurations $\mathbf{q}_0, \mathbf{q}_1$ from $\mathbf{w}_0, \mathbf{w}_1$ with the help of the inverse kinematics.
2. Calculation of the center in joint space:

$$\mathbf{q}_m = \frac{\mathbf{q}_0 + \mathbf{q}_1}{2}$$

Motion along a line $\langle \mathbf{w}_0, \mathbf{w}_1 \rangle$ (cont.)

3. Calculation of the corresponding point of \mathbf{q}_m in the workspace with usage of direct kinematics:

$$\mathbf{w}_m = W(\mathbf{q}_m)$$

4. Calculation of the center in the workspace:

$$\mathbf{w}_M = \frac{\mathbf{w}_0 + \mathbf{w}_1}{2}$$

5. If the deviation $\|\mathbf{w}_m - \mathbf{w}_M\| \geq \epsilon$, then cancel; else add the \mathbf{w}_M as node point between \mathbf{w}_0 and \mathbf{w}_1 .
6. Recursive application of the algorithm for two new segments $(\mathbf{w}_0, \mathbf{w}_M)$ und $(\mathbf{w}_M, \mathbf{w}_1)$.



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